

#### **Poster EGU2015-791**

# Introduction

Underground coal gasification (UCG) can allow to develop coal deposits not economically mineable by conventional methods due to large depths or complex geology. Even though, economic potentials are generally expected to be high, potential environmental impacts, comprising ground surface subsidence and groundwater pollution, have to be assessed on a site-specific basis. Thereto, we developed a coupled thermo-mechanical model to calculate permeability changes in the vicinity of an UCG reactor. Our simulation results allow for an assessment of fluid flow into and out of a UCG reactor during operation and in the postabandonment phase.

## Underground coal gasification

- UCG has the potential to **increase** world-wide coal reserves by utilization of deposits not mineable by conventional methods [1].
- UCG produces a **high-calorific** synthesis gas for electricity generation and/or chemical feedstock production [2,3].
- Ground subsidence and groundwater pollution are potential environmental impacts [1].



# Model domain and boundary conditions

- 2D model was discretized by about **3,000 elements** with unstructured mesh and four reactor sizes applied with stepwise reactor excavation (shapes 1-4 in right figure).
- Stress boundary condition at model top to represent overburden load and fixed velocity boundary conditions at lateral and bottom boundaries.





# Do we have to consider temperature-dependent material properties in large-scale environmental impact assessments of UCG?

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# Model parameterization

# H2 / CH4 CO2 / CO asification area

### Model parameterization based on available literature data [3-5].

Input parameter		Unit	Sandstone	Coal
Mechanical parameters				
Elastic modulus ( <i>E</i> )	f(T)	GPa	4	2
Tensile strength ( $\sigma_t$ )	f(T)	МРа	5	5
Friction angle ( $\phi$ )	Constant for rock	o	32	20
Cohesion (c)	Constant for rock	MPa	5	1
Poisson ratio (v)	Constant	-	0.35	0.44
Density (ρ)	Constant	kg/m³	2,200	1,300
Thermal parameters				
Linear thermal expansion coefficient (a)	f(T)	K-1	1.6x10 <sup>-5</sup>	5.0x10 <sup>-6</sup>
Specific heat capacity ( $C_P$ )	f(T)	J/kg K	1,363	2,000
Thermal conductivity ( $\lambda$ )	f(T)	W/m/K	2.30	0.23

#### Trend of **thermo-mechanical** sandstone and coal property development as f(T) shows **high temperature dependency**.

#### · 2.0 Temperature (°C) Drying zone **Drying and Pyrolysis zone** 200 - 900°C - Release of volatile matter > 900°C 1.2 coal loses its moisture 550 - 900°C \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ \_ 100 200 300 400 500 600 700 800 900 Temperature (°C)

ncrease of a above 200 °

# Summary and Conclusions

- Thermo-mechanical rock behavior of sandstone and bituminous coal is mainly influenced by thermal expansion coefficient, tensile strength and elastic modulus.
- Permeability changes derived from volumetric strain increments show negligible differences for temperature dependent and -independent parameters.
- Near-field models require temperature-dependent parameters, while far-field models can benefit from higher computational efficiency by neglecting temperature-dependence.







#### References

[1] Burton, E., Friedmann, J., Upadhye R. (2006) Best practice in underground coal gasification. Technical Report. LLNL, US Department of Energy, CA. [2] Nakaten, N. C., Schlüter, R., Azzam, R., Kempka, T. (2014) Energy 66:779-790. [3] Tian, H., Kempka, T., Xu, N.-X., Ziegler, M. (2012) Rock Mech Rock Eng, 45(6):1113-1117. [4] Tian, H., Kempka, T., Yu, S., Ziegler, M. (2015) Rock Mech Rock Eng, 7 p. Article in Press. doi:10.1007/s00603-015-0724-z. [5] Otto, C., Kempka, T. (2015) Submitted to Energies.

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# Simulation results



- Permeability is expressed as function of volumetric strain increment.
- Regions of **high temperature** (black solid line: temperature  $\geq 200 \,^{\circ}$ C) experience positive volumetric strain increments in reactor vicinity.
- Permeability changes (normalized) show negligible differences for temperaturedependent and -independent parameters.





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